

# MAPPING OF LATERAL SPREAD DISPLACEMENT HAZARD, WEBER COUNTY, UTAH

by

Steven F. Bartlett

Daniel Gillins

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EERI

# Outline

- Modification to Lateral Spread Model
- Interpreting and Use CPT Data in Revised Model
- Monte Carlo Method
- Mapping Inputs
- Map Examples

# Youd et al. (2002) Empirical Model

$$\text{Log}D_H = b_o + b_{off}\alpha + b_1M + b_2\text{Log}R^* + b_3R + b_4\text{Log}W + b_5\text{Log}S + b_6\text{Log}T_{15} + b_7\text{Log}(100 - F_{15}) + b_8\text{Log}(D50_{15} + 0.1 \text{ mm})$$

## ⊙ Seismic Factors

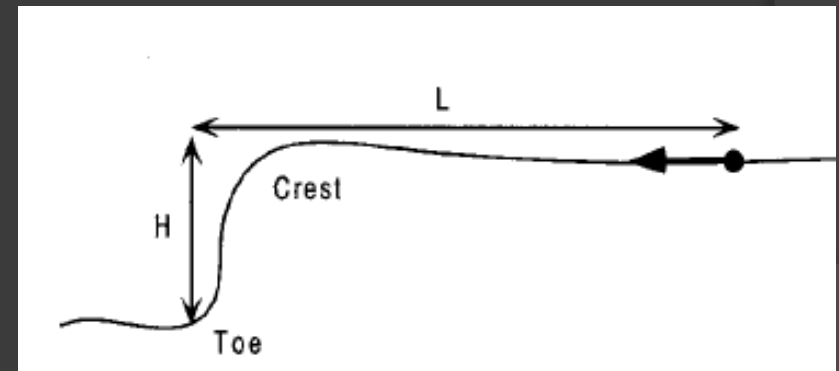
- $M, R$

## ⊙ Topographic Factors

- $W, S$

## ⊙ Geotechnical Factors

- $T_{15}, F_{15}, D50_{15}$



Free-face ratio:  $W (\%) = H / L * 100$

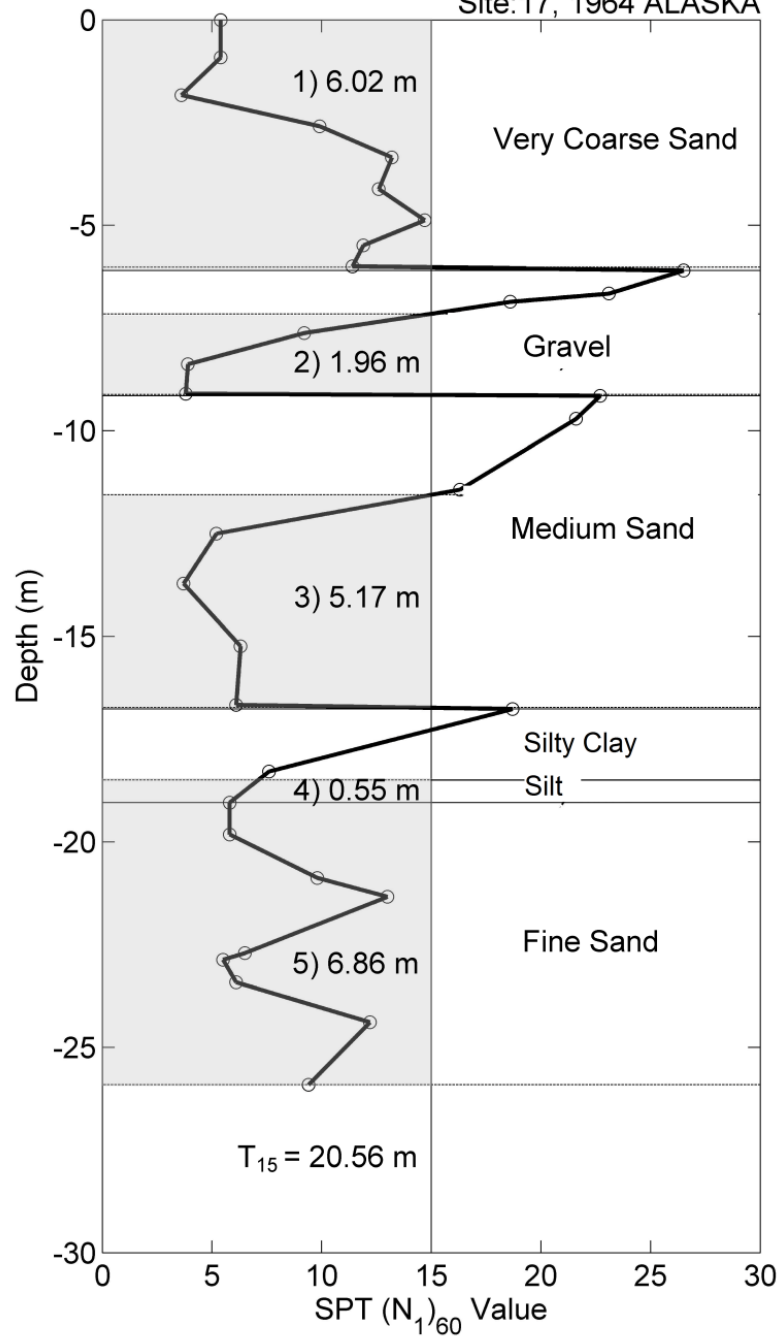
# New Empirical Model

$$\text{Log}D_H = b_o + b_{\text{off}}\alpha + b_1M + b_2\text{Log}R^* + b_3R + b_4\text{Log}W + b_5\text{Log}S + b_6\text{Log}T_{15} + a_1x_1 + a_2x_2 + a_3x_3 + a_4x_4 + a_5x_5$$

$x_i$  = the portion (decimal fraction) of  $T_{15}$  in a borehole that has a soil index corresponding to the table below

Soil Index (SI)	Typical Soil Description in Case History Database	General USCS Symbol
1	Silty gravel, fine gravel	GM
2	Coarse sand, sand and gravel	GM-SP
3	Medium to fine sand, sand with some silt	SP-SM
4	Fine to very fine sand, silty sand	SM
5	Low plasticity silt, sandy silt	ML
6	Clay (not liquefiable)	CL-CH

Site:17, 1964 ALASKA

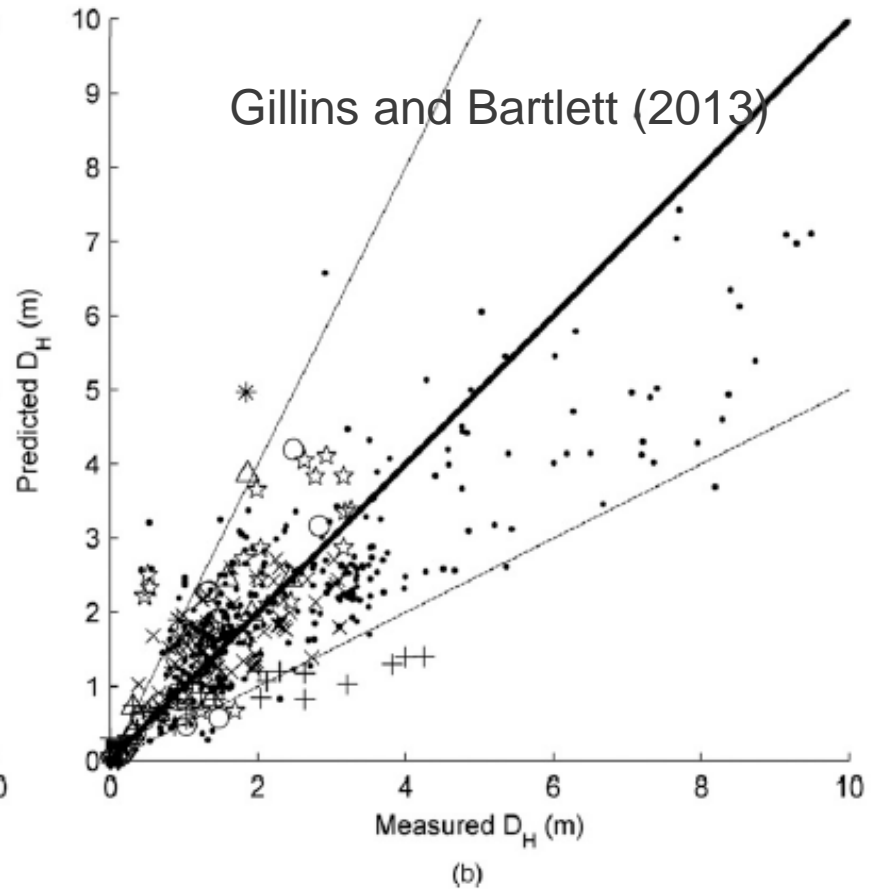
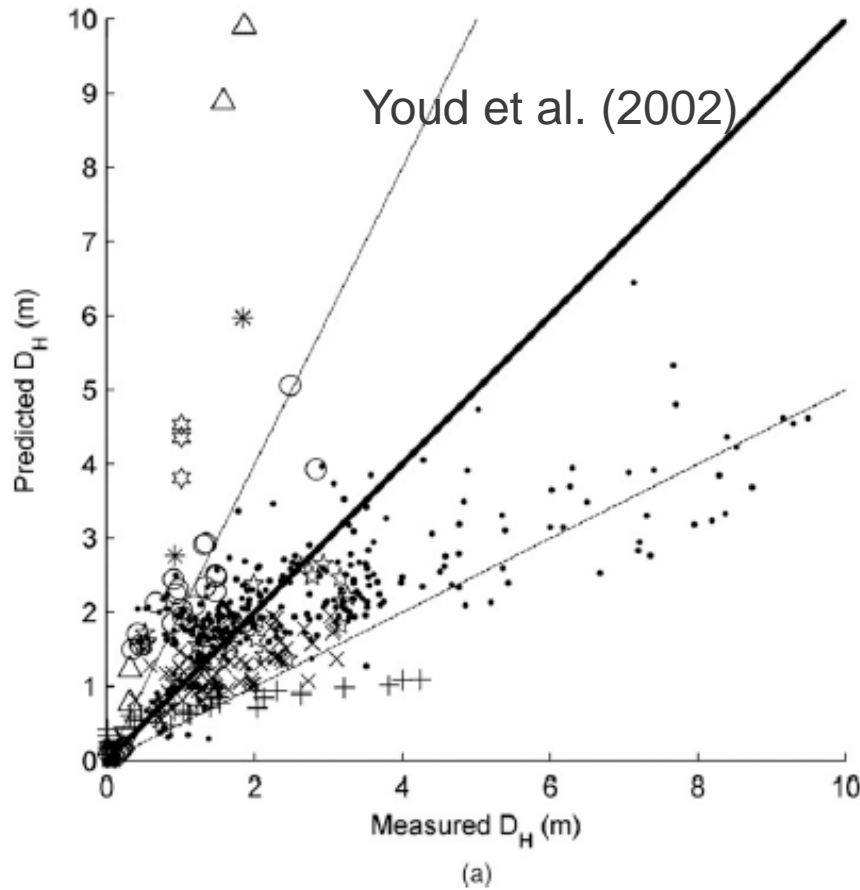


sented as a decimal. For example, the borehole plotted in Fig. 2 has  $x_1 = 1.96/20.6 = 0.10$ ,  $x_2 = 6.02/20.6 = 0.29$ ,  $x_3 = 0.25$ ,  $x_4 = 0.33$ , and  $x_5 = 0.03$ . Of course, the sum of all values of  $x$  in the borehole equals 1.

# Comparing the Models

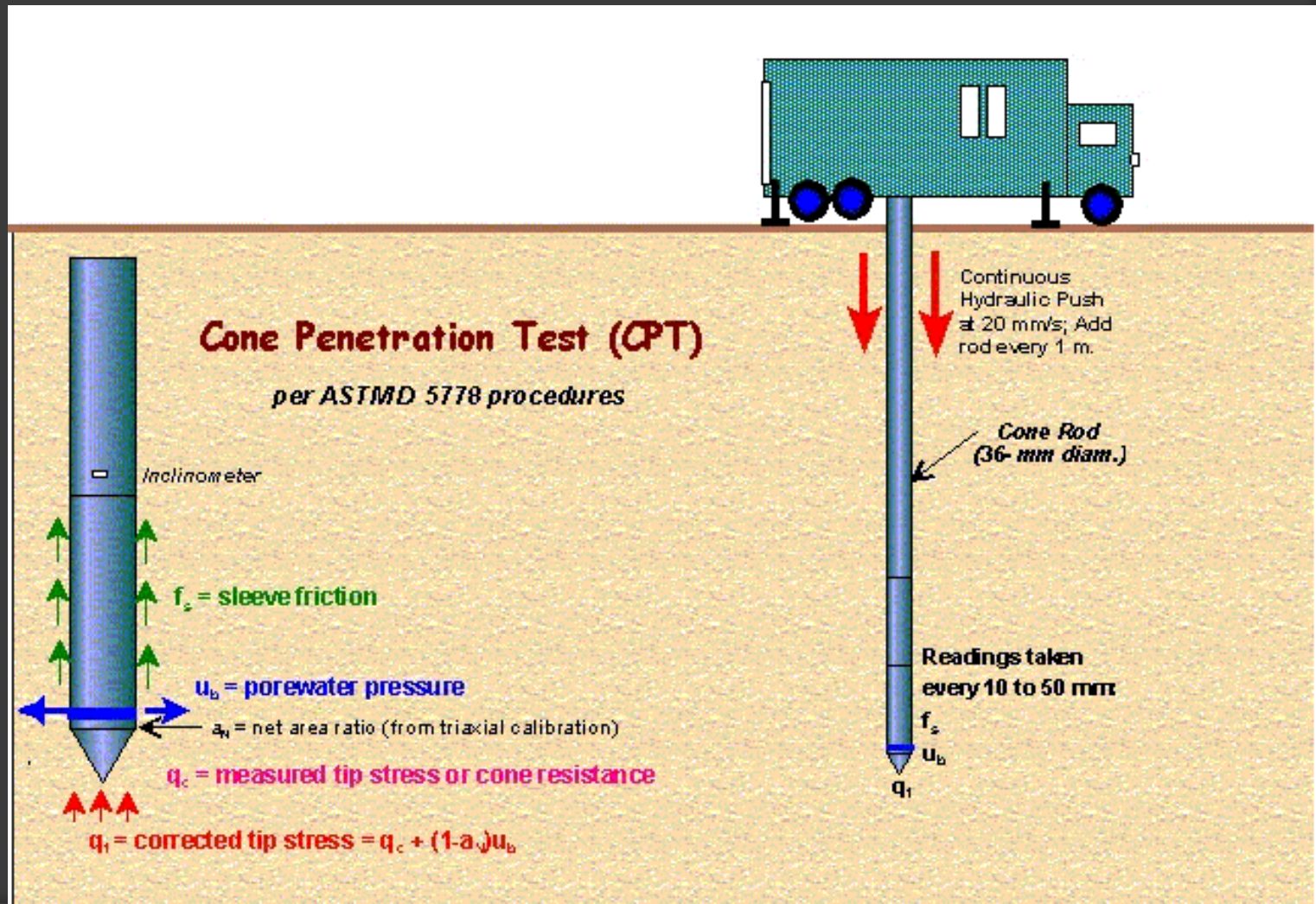
Model	$R^2$ (%)	$MSE$	$\sigma_{\log DH}$	P-Value
Full: Youd et al. (2002)	83.6	0.0388	0.1970	0.000
Reduced: no $F_{15}$ or $D50_{15}$	66.6	0.0785	0.2802	0.000
New: with soil type terms	80.0	0.0476	0.2182	0.000

* 1906 San Francisco	☆ 1971 San Fernando	◇ 1987 Superstition Hills	
△ 1964 Alaska	+ 1979 Imperial Valley	□ Ambraseys' Data	○ 1995 Kobe
• 1964 Niigata	× 1983 Nihonkai-Chubu	☆ 1983 Borah Peak, Idaho	▽ 1989 Loma Prieta



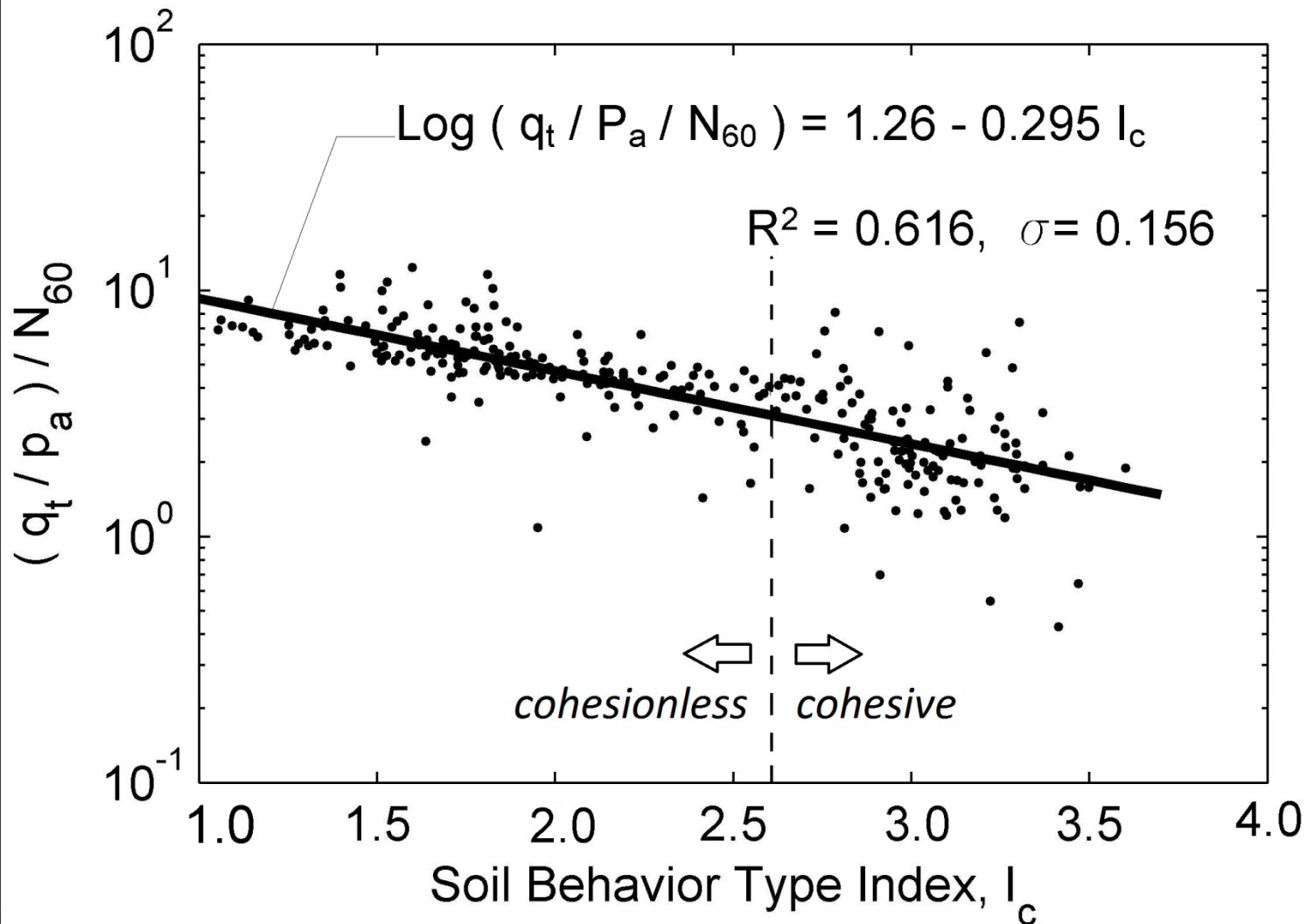
**Fig. 1.** Predicted lateral spread displacement using (a) Eq. (3) or (b) Eq. (4), versus measured lateral spread displacement from the case history database of Youd et al. (2002)

# Cone Penetrometer Test (CPT)





# Estimating $N_{1,60}$ from CPT Data



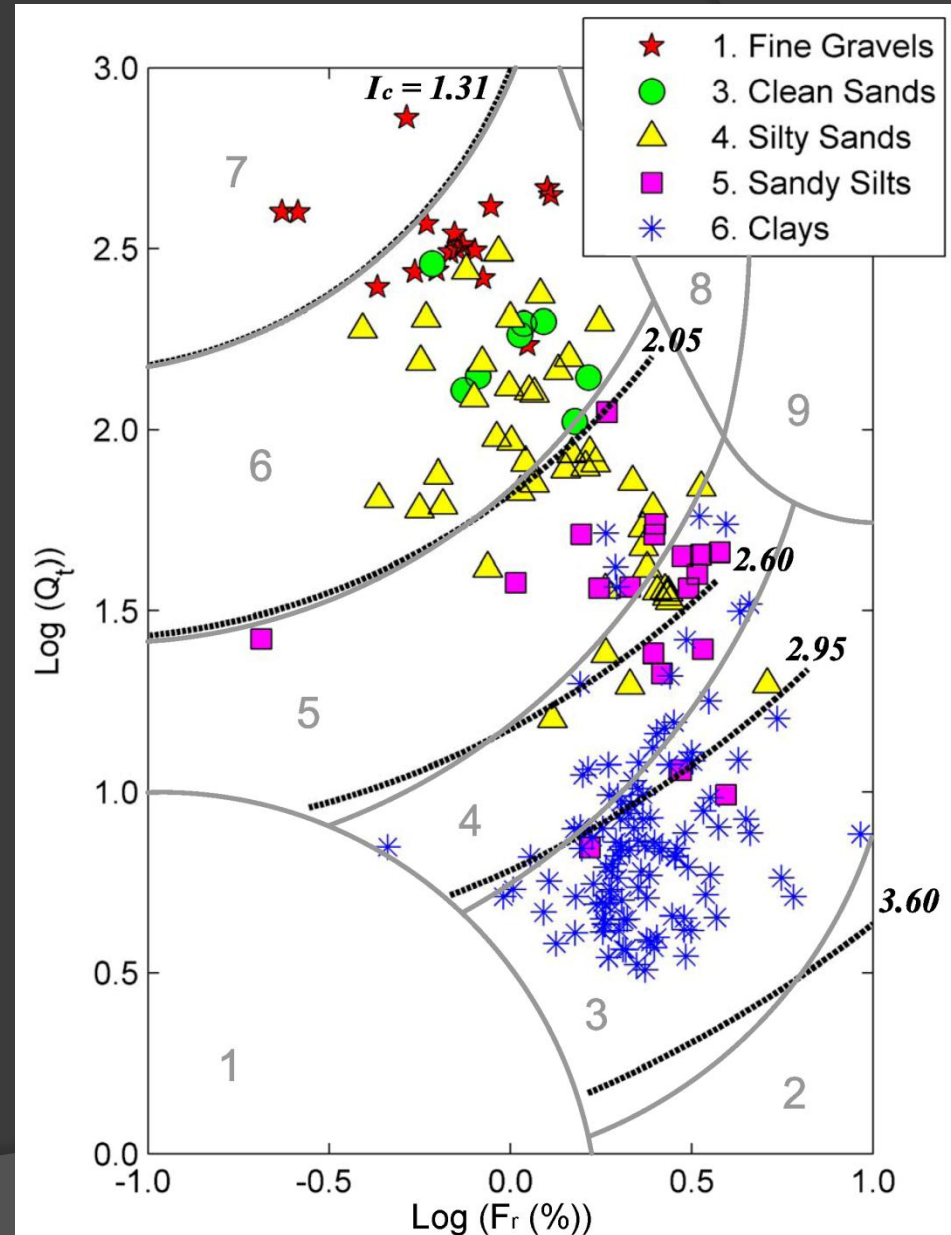
# Estimating $x_i$ Variables with CPT

Zone	Soil Behaviour Type (SBT)
1	<i>Sensitive fine-grained</i>
2	<i>Clay - organic soil</i>
3	<i>Clays: clay to silty clay</i>
4	<i>Silt mixtures: clayey silt &amp; silty clay</i>
5	<i>Sand mixtures: silty sand to sandy silt</i>
6	<i>Sands: clean sands to silty sands</i>
7	<i>Dense sand to gravelly sand</i>
8	<i>Stiff sand to clayey sand*</i>
9	<i>Stiff fine-grained*</i>

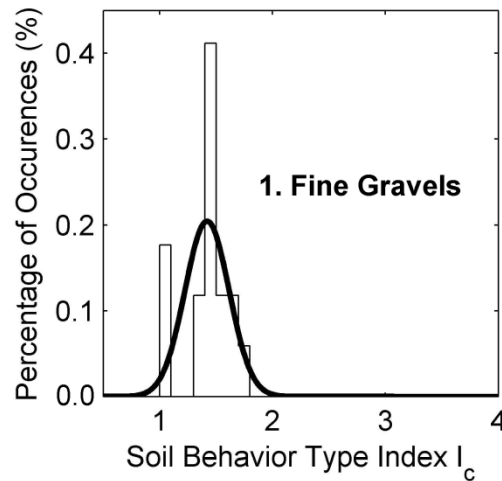
\* Overconsolidated or cemented

$$I_c = [(3.47 - \text{Log} Q_{tn})^2 + (\text{Log} F_r + 1.22)^2]^{0.5}$$

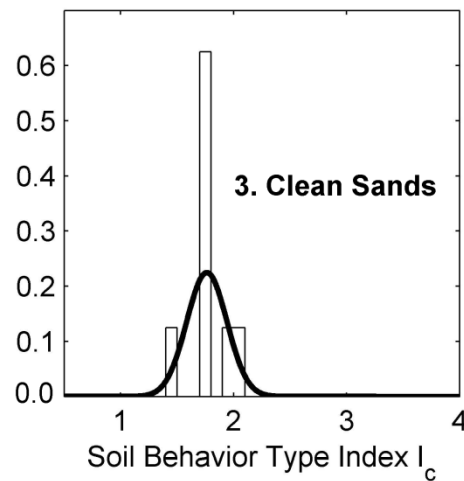
Robertson (1990) Soil Behavior Type Chart  
Boundaries of each zone estimated by circles with radius =  $I_c$



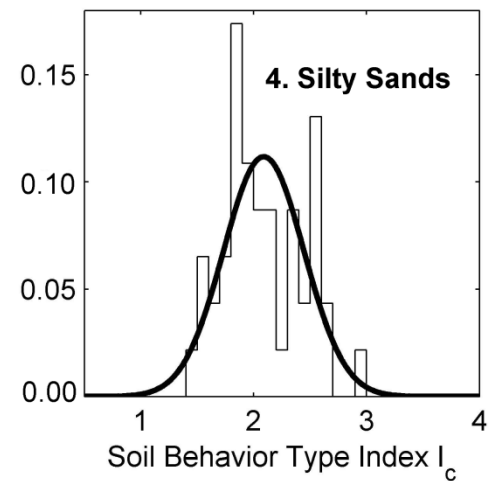
# Histograms of $I_c$ for each $S_l$



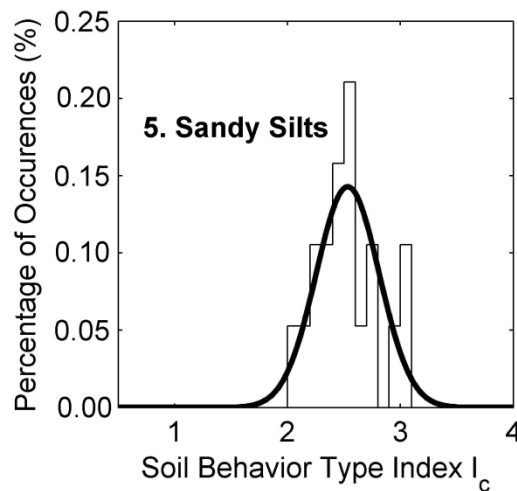
(a)



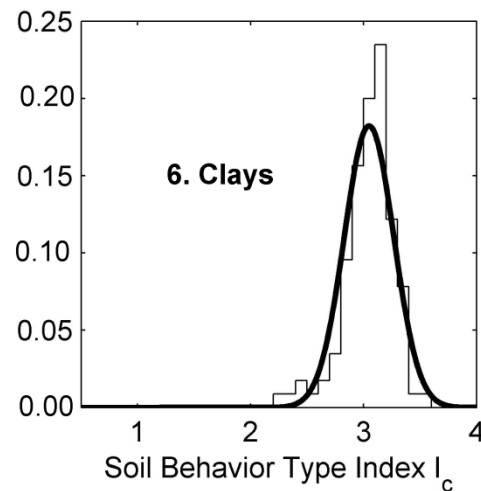
(b)



(c)

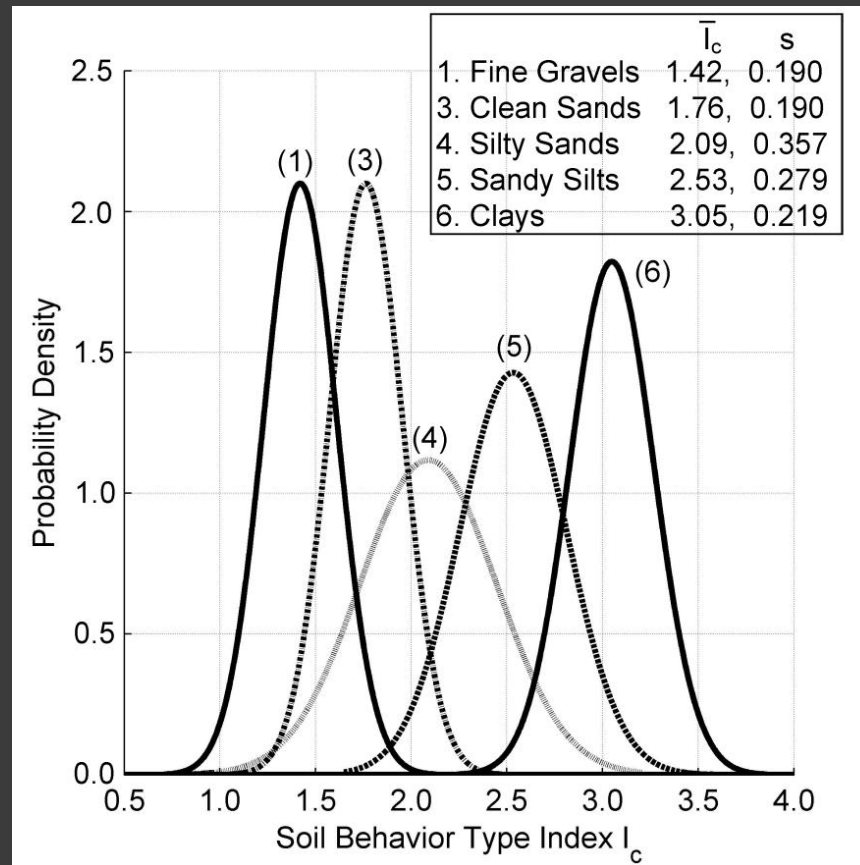


(d)



(e)

# Charts to Estimate $S_I$ given $I_c$



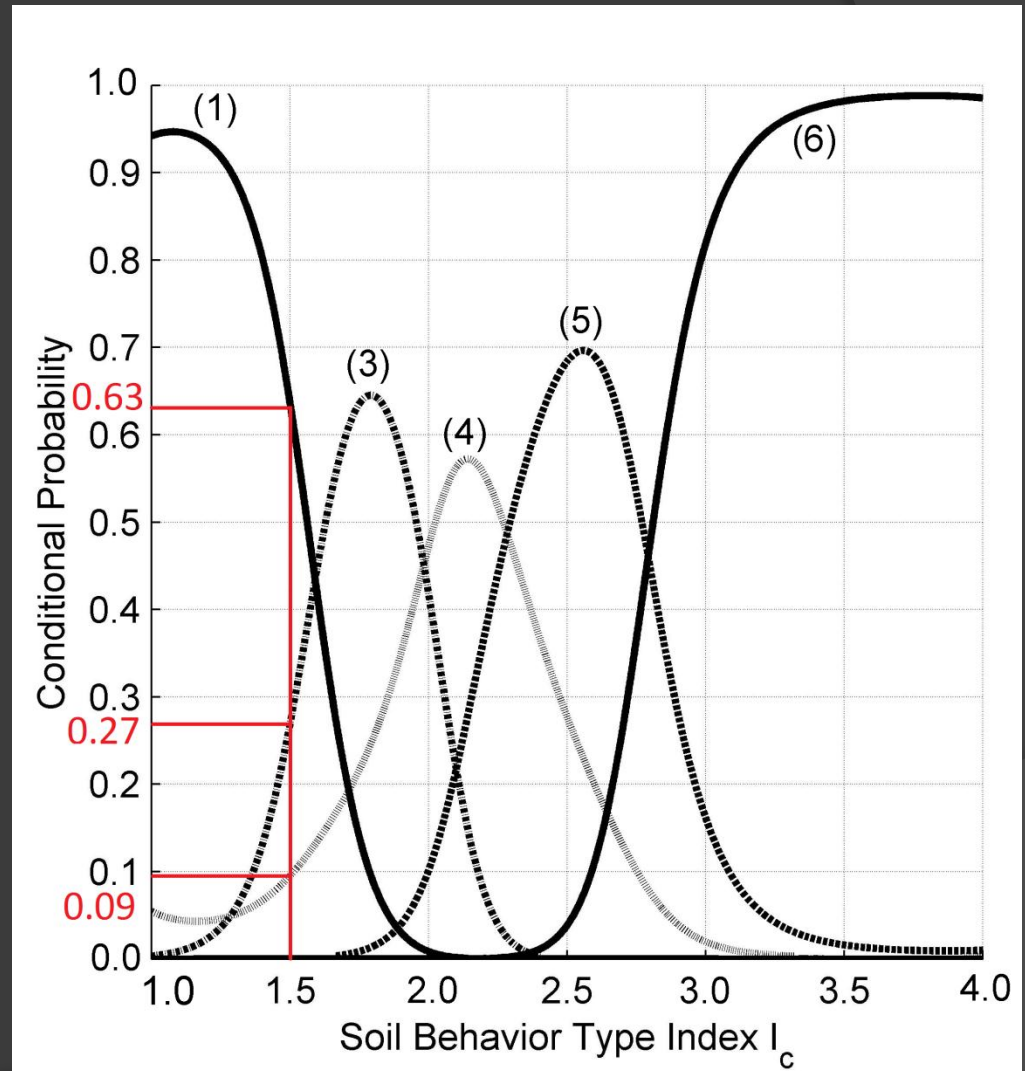
Recommended normal probability  
density functions; Weber County

# Example 1

Find probability that:  
 $SI = 1$  (i.e., fine gravel)  
given  $I_c = 1.5$

$$P(SI = i \mid I_c = 1.5):$$

$i$	$P$
1. Fine Gravels	0.63
3. Clean Sands	0.27
4. Silty Sands	0.09
5. Sandy Silts	0.00
6. Clays	0.00

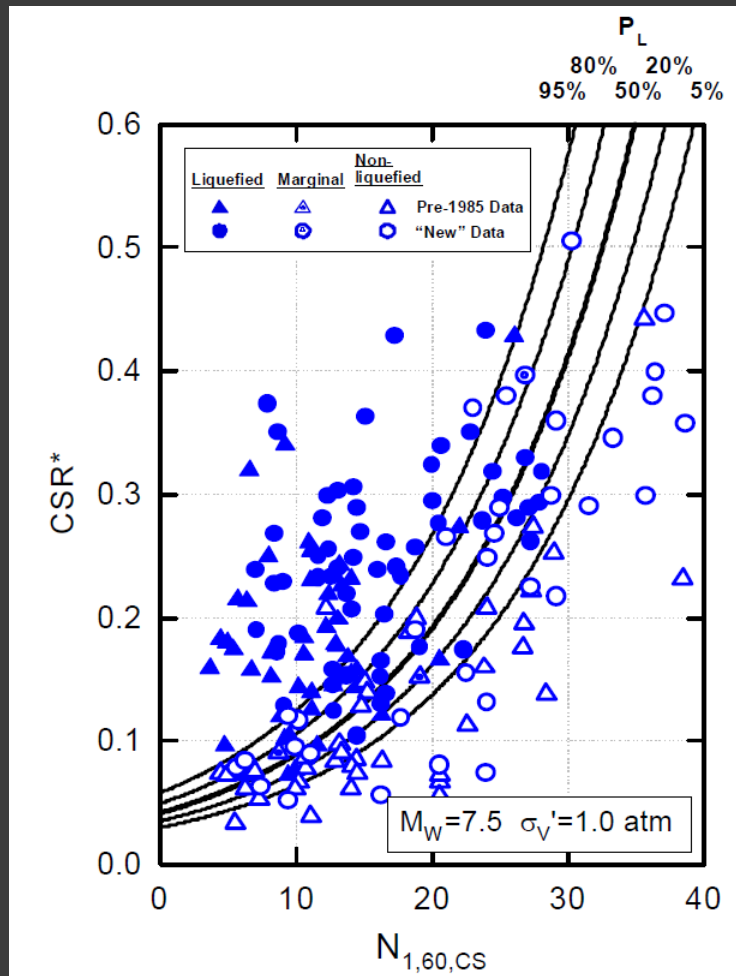


# Probabilistic Framework

$$P[D_H > y] = P[D_H > y | L] \cdot P_L$$

1. Select a threshold distance,  $y$
2. Find  $P[D_H > y | L]$  using new empirical model
3. Find  $P_L$  from liquefaction potential curves of Cetin et al. (2004) and Moss et al. (2006)

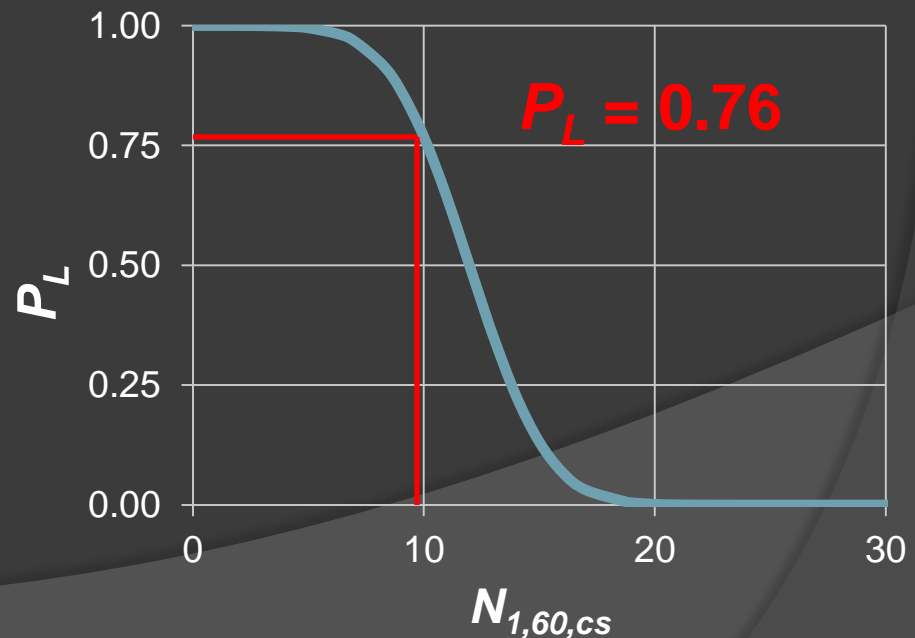
# Example 2



SPT-based Liquefaction Potential Curves (Cetin et al., 2004)

Find  $P[ D_H > 1 \text{ m}]$  given:

- $CSR = 0.1; N_{1,60,cs} = 10$
- $M = 7.5; R = 20 \text{ km}$
- $S = 0.5 \%$
- $T_{15,cs} = 1 \text{ m}; \sigma'_v = 1 \text{ atm}$

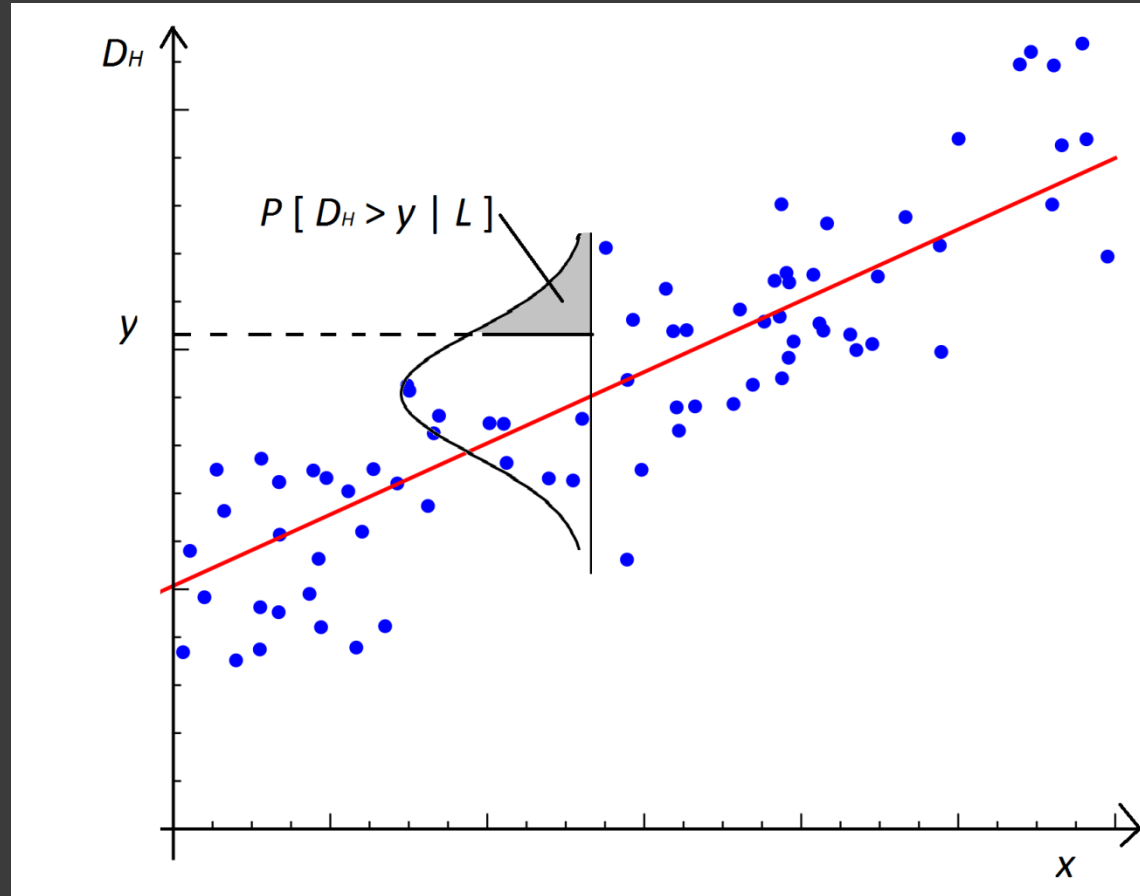


# Example 2 (cont.)

$$P[D_H > y \mid L] = \Phi\left(-\frac{\text{Log}(y) - \overline{\text{Log}(D_H)}}{\sigma_{\text{Log}(D_H)}}\right)$$

$$= \Phi(-z)$$

$$= \underline{0.33}$$



$$P[D_H > y] = (0.33) * (0.76) = \underline{0.25}$$

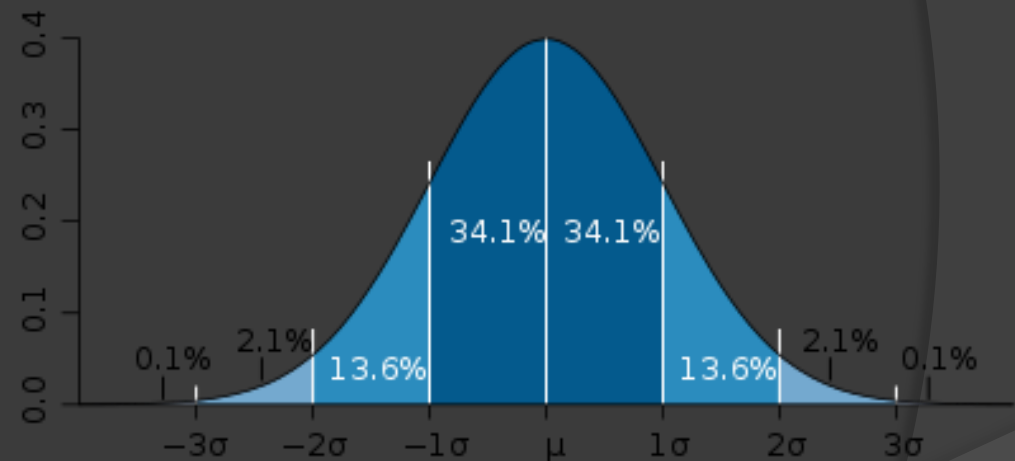


“Simple calculations based on a range of variables are better than elaborate ones based on limited input.”

-Ralph B. Peck

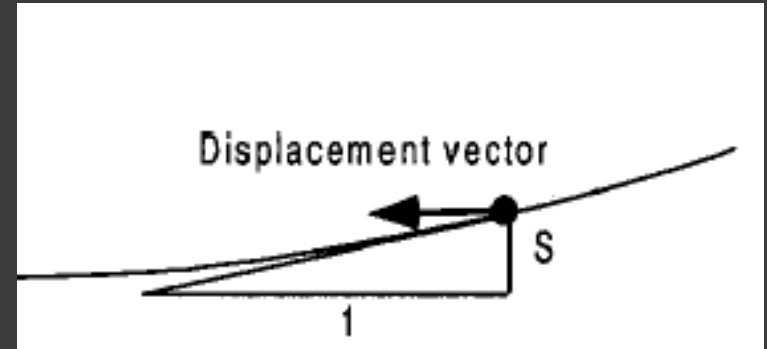
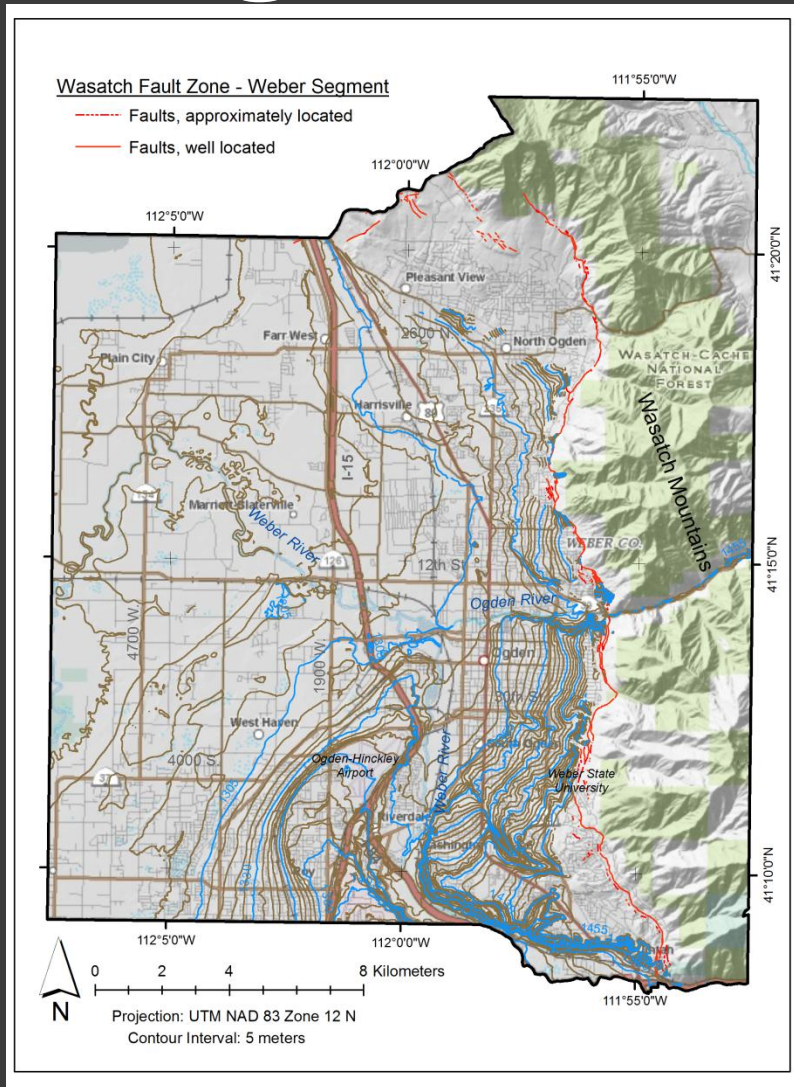
# Monte Carlo Technique

- ⦿ Used when:
  - Unable to compute results deterministically
  - Systems have many degrees of freedom
  - Modeling phenomena with significant uncertainty
- 1) Define a domain of inputs
- 2) Generate inputs randomly from a probability distribution over the domain;
- 3) Perform a deterministic computation on the inputs;
- 4) Aggregate the results to define the median values and their uncertainty

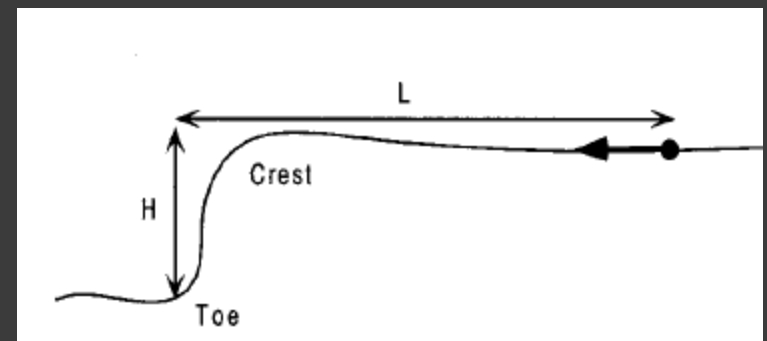


The Normal Distribution

# Topographic Variations



Percent ground slope:  $S (\%)$

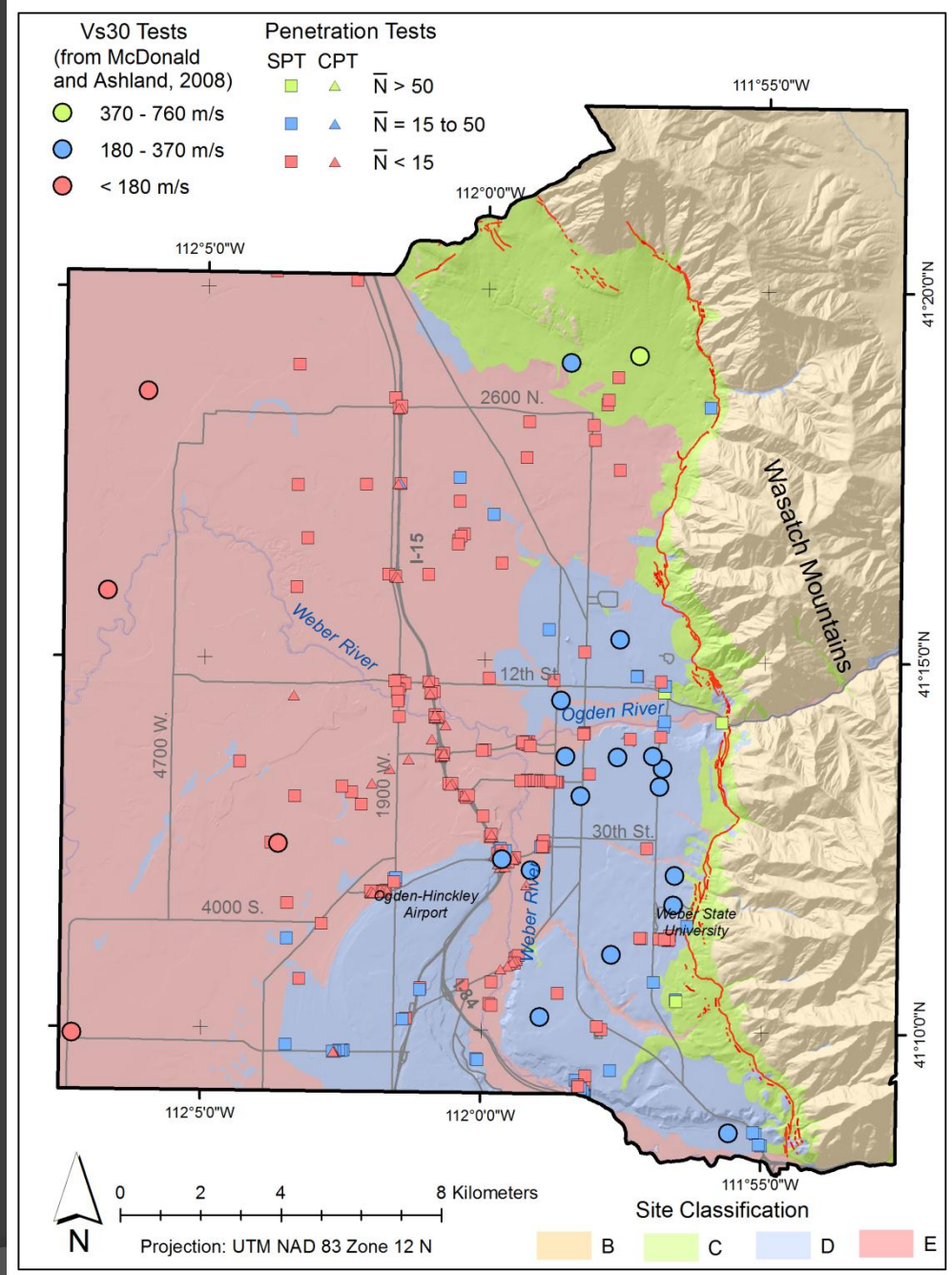


Free-face ratio:  $W (\%) = H / L * 100$

Contours Based on Digital  
Elevation Model (DEM) from  
USGS National Elevation Dataset

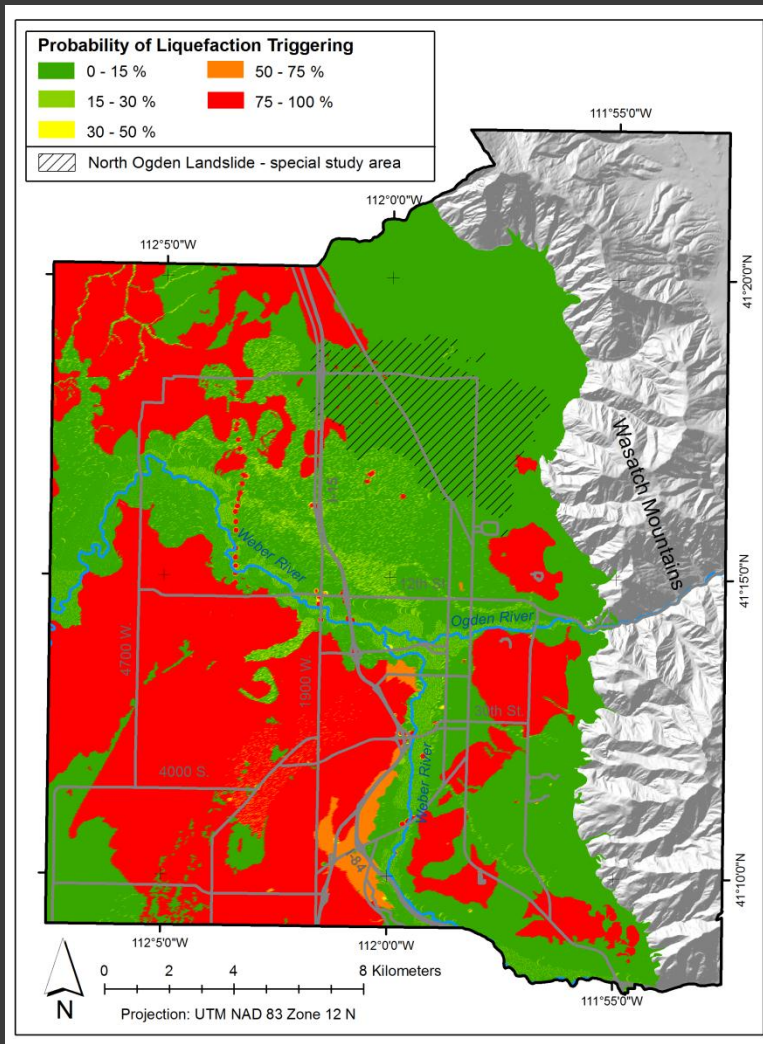
# Seismic Inputs

- Mean seismic variables from interactive deaggregation of the seismic hazard
- Seismic hazard based on 2008 source and attenuation models of the National Seismic Hazard Mapping Project (Peterson et al., 2008)

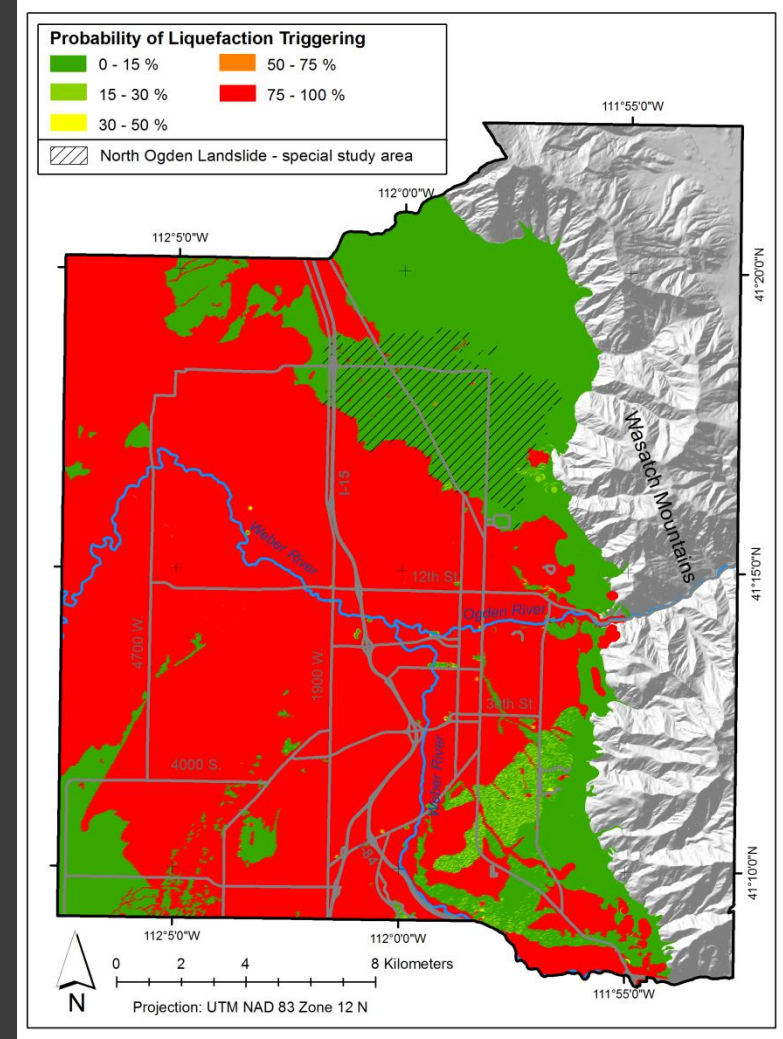




# Liquefaction Triggering Maps

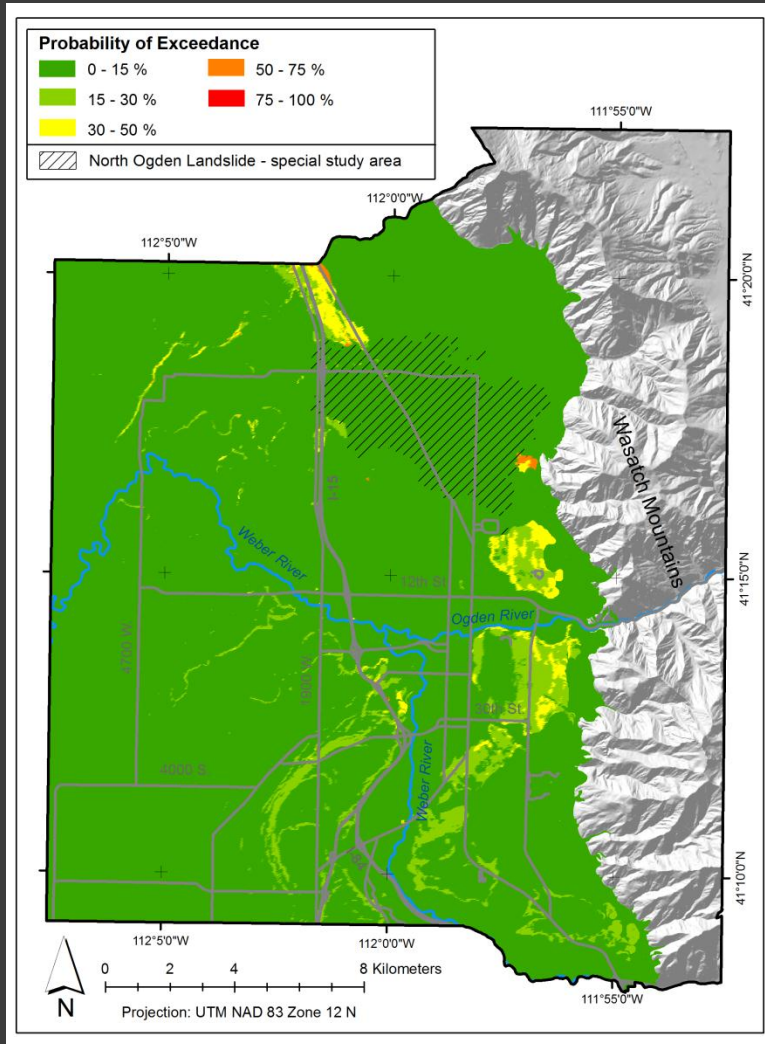


Median probabilities of  $P_L$ , 500-year seismic event

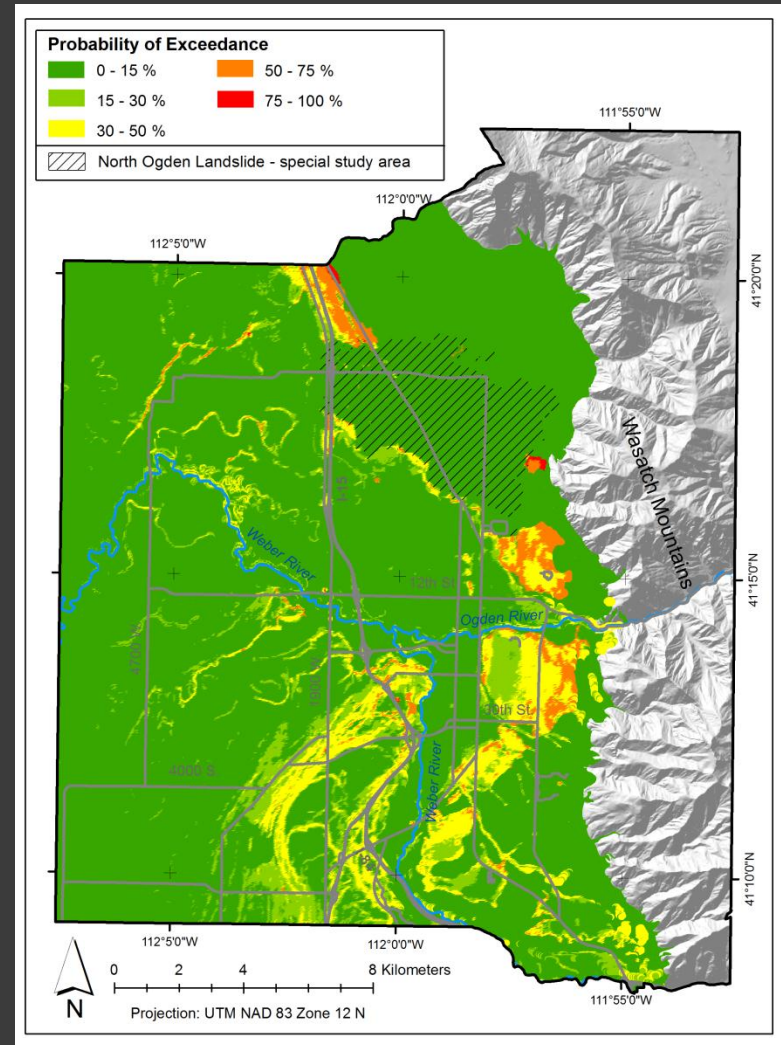


Median probabilities of  $P_L$ , 2,500-year seismic event

# Lateral Spread Hazard Maps



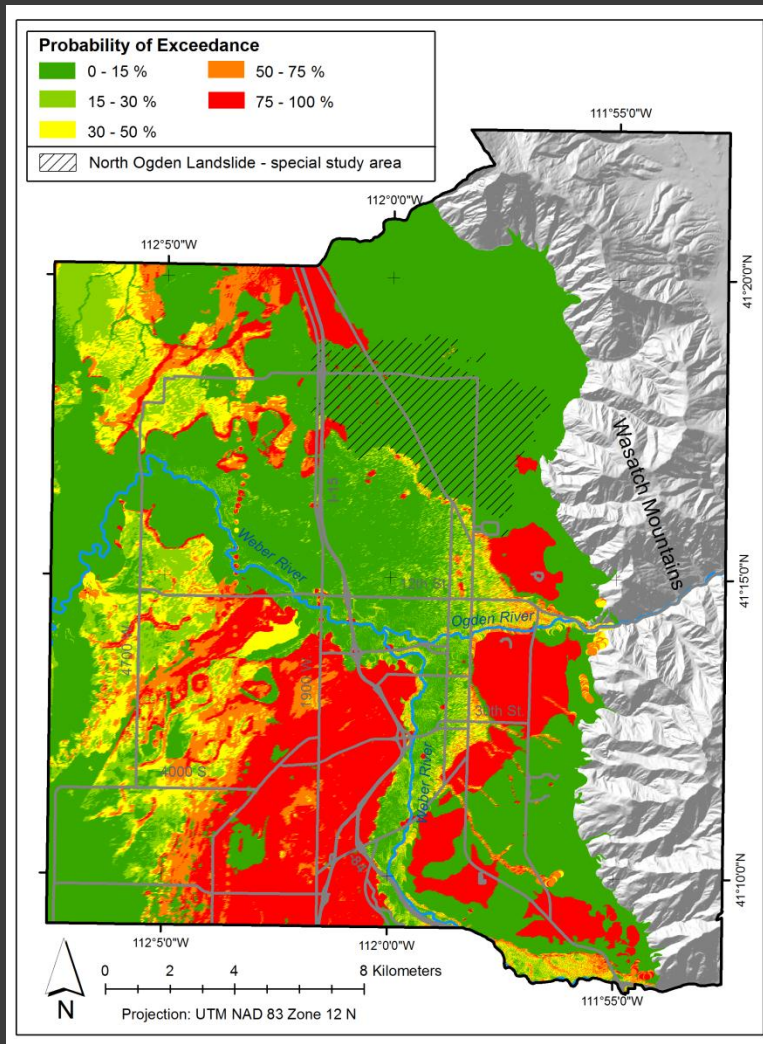
Median probabilities of exceeding  
0.3 m, 500-year event



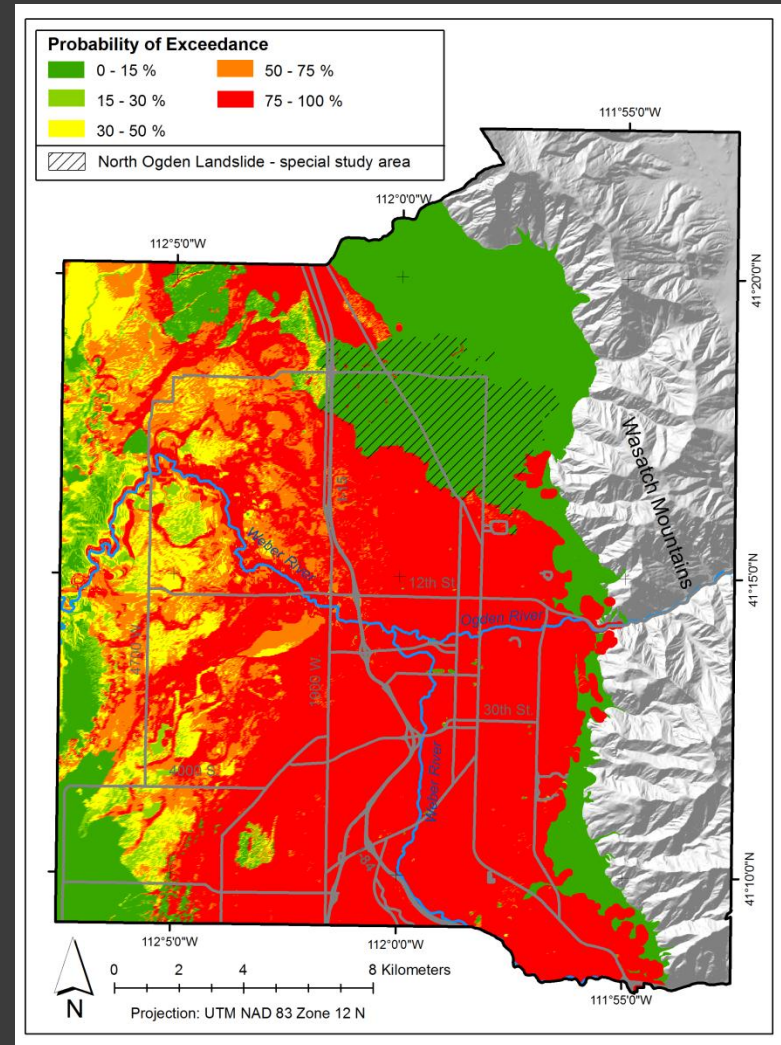
84<sup>th</sup> percentile probabilities, of  
exceeding 0.3 m, 500-year event



# Lateral Spread Hazard Maps



Median probabilities of exceeding  
0.3 m, 2,500-year event



84<sup>th</sup> percentile probabilities, of  
exceeding 0.3 m, 2,500-year event

# For more information:

<http://www.civil.utah.edu/~bartlett/ULAG/>

## Multilinear Regression Equations for Predicting Lateral Spread Displacement from Soil Type and Cone Penetration Test Data

Daniel T. Gillins, Ph.D., M.ASCE<sup>1</sup>; and Steven F. Bartlett, Ph.D., M.ASCE<sup>2</sup>

<sup>1</sup>Assistant Professor, School of Civil and Construction Engineering, Oregon State Univ., Corvallis, OR 97331 (corresponding author). E-mail: [dan.gillins@oregonstate.edu](mailto:dan.gillins@oregonstate.edu)

<sup>2</sup>Associate Professor, Dept. of Civil and Environmental Engineering, Univ. of Utah, Salt Lake City, UT 84112. E-mail: [bartlett@civil.utah.edu](mailto:bartlett@civil.utah.edu)

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